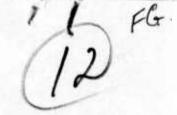
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80 West End Avenue / New York, New York 10023 / (212) 873-4000

23 January 1976

TECHNICAL REPORT T-2/306-3-14

PRESENT STATUS OF THE RRI SLANT-PATH

ABSORPTION MODEL (SLAM) COMPUTER PROGRAM

By D. Koppel

Prepared for

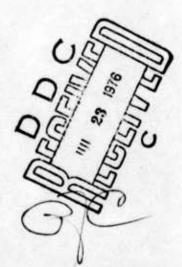
Commanding General
U. S. Army Missile Command
Redstone Arsenal, Alabama 35809

Contract No. DAAH01-74-C-0419, Mod. P00009

Sponsored by

Advanced Research Projects Agency 1400 Wilson Boulevard Arlington, Virginia 22209

ARPA Order No. 2281



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AUTHORIZATION

This report describes work performed at Riverside Research Institute by D. Koppel with the assistance of M. Greenebaum and S. Rosenberg. The report was written by D. Koppel.

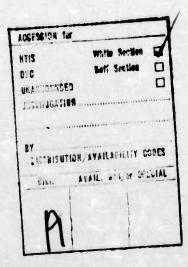
This project is sponsored by the Advanced Research Projects Agency of the Department of Defense and administered by the U. S. Army Missile Command, Redstone Arsenal, Alabama, under Contract No. DAAHO1-74-C-0419, Mod. P00009.

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M. Arm Research Director



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ABSTRACT

A computer program (SLAM) is described which calculates the attenuation by air of microwave and submillimeter radiation. Besides the horizontal attenuation, the vertical attenuation from various levels down to the ground and out into space is calculated for a fixed frequency. The line profile and atmospheric model can be selected from among several. Comparison is made with other calculations, and with experiments. Possibilities for improving the program are discussed.



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TECHNICAL REPORT T-2/306-3-14 PRESENT STATUS OF THE RRI SLANT - PATH ABSORPTION MODEL (SLAM) COMPUTER PROGRAM

I. INTRODUCTION

DARPA, RRI has developed a computer program to calculate atmospheric attenuation in the microwave and submillimeter regions of the electromagnetic spectrum. This program is intended for analyzing communications systems and other applications in this spectral region not only at ground level but also with transmitters and receivers at higher altitudes. Hence, emphasis has been placed on calculating the total attenuation down to the ground and out into space at any given frequency, at a set of reasonably spaced atmospheric levels. The program is written in FORTRAN and may be looked upon as a modification of a program originated by McClatchey, et. al. of AFCRL.

The inputs to the program consist of an atmospheric model, a spectral line compilation, and a control file giving the choice of parameters to be used in the calculations. Currently six atmospheric models are available for use. These are the "Tropical," "Midlatitude Summer," "Midlatitude Winter," "fubartic Summer," "Subarctic Winter," and "U.S. Standard Atmosphere, 1962" all as formulated by McClatchey, et. al. 3. The "Midlatitude Winter" model is reproduced in Table I. This model gives the pressure, temperature, and water vapor and ozone contents as a function of altitude. The other species currently represented in the spectral line compilation, namely oxygen and carbon monoxide, are assumed to have constant mixing ratios. Other atmospheric models can be used by changing the input file. The spectral line compilation

TABLE I
MIDLATITUDE WINTER MODEL USED IN SLAM PROGRAM

HEIGHT	PRESSURE (MBAR)	TEMP	WAT	ER 14#3)	-	ZONE
0.	1.0180E+03	272.2	3.5	E+00	4.00	00E=05
1.	8 . 973 E+02	268.7	2.5	E+00	5.4	E-05
2.	7.897 E+02	265.2	1.8	E+00	419	E-05
3.	6.938 E+02	261.7	1.2	E+00	4.9	E-05
4.	6.081 E+02	255.7	6.6	E-01	4.9	E-05
5.	5.313 E+02	249.7	3.8	E-01	5.8	E-05
6.	4.627 E+02	243.7	2.1	E-01	614	E-05
7.	4.016 E+02	237.7	8.5	E-05	7.7	E-05
8.	3.473 E+02	231.7	3.5	E-05	9.0	E-08
9.	2.992 E+02	225.7	1.6	E-02	1.2	E-04
10.	2.568 E+02	219.7	7.5	E-03	1.6	E-04
11.	2.199 E+02	219.2	6.9	E-03	2.1	E-04
12.	1 . 882 E+02	218.7	6.0	E-03	2.6	E-04
13.	1.610 E+02	218.2	1.8	E-03	3.0	E-04
14.	1 . 378 E+02	217.7	1.0	E-03	3.2	E-04
15.	1 - 178 E+02	217.2	7.6	E-04	314	E-04
16.	1.007 E+02	216.7	6.4	E-04	316	E-04
17.	8.610 E+01	216.2		E-04	3.9	E-04
18.	7.350 E+01	215.7	5.0	E-04	4+1	E-04
19.	6.280 E+01	215.2		E-04	4.3	E-04
20.	5.370 E+01	215.2	4.5	E-04	4.5	E-04
21.	4+580 E+01	215.2	5.1	E-04	413	E-04
22.	3.910 E+01	215.2	5.1	E-04	4.3	E-04
23.	3.340 E+01	215.2	5.4	E-04	3.9	E-04
24.	2.860 E+01	215.2		E-04	3.6	E-04
25.	2.430 E+01	215.2		E-04	314	E-04
30.	1-110 E+01	217.4	3.6	E-04	1.9	E-04
35.	5-180 E+00	227.8		E-04	9.2	E-05
40.	2.530 E+00	243.2	_	E-05	4+1	E-05
45.	1.290 E+00	258.5		E-05	1.3	E-05
50.	6.820 E-01	265.7	6.3	E-06	4.3	E-06
70.	4.670 E-02	230.7		E-07	8.6	E-08
100.		210.2				

used has been taken in large part from the first section of a magnetic tape obtained from AFCRL4. In most of the 0 to 550 cm⁻¹ spectral region under consideration, i.e., in the "pure rotation" region below 430 cm⁻¹, this tape includes only water, ozone, and the microwave spectrum of oxygen. Consequently, this compilation has been modified by adding the results recently obtained at RRI on the submillimeter and microwave spectrum of oxygen and on the rotational spectrum of carbon monoxide. 6 (The oxygen lines were added for three isotopic species: 160160.160180 and 180180. Both the ground vibrational level and the first vibrationally excited state were taken into accound for 160160.) A sample of the compilation is shown in Table II. The first column gives the frequency in cm⁻¹; the second column, the (modified) integrated line strength at 296K, in cm⁻¹/molecules cm⁻² (modification described below); the third column, the pressure coefficient of the line half-width in cm-1/atm; the fourth column, the energy of the lower state in cm⁻¹; the fifth column, the date (month and year) of insertion into the file; the sixth column, the isotope concerned (e.e., 68 is 016018); and the seventh column. the molecular constituent, the integers M=1,3,5,7 standing for water vapor, ozone, carbon monoxide, and oxygen, respectively.

The data on the tape received from AFCRL was first converted to the 9-track format required by the Xerox Sigma 9 computer and then was placed into a magnetic disc file and converted from BCD to binary format (for increased speed). The control file (Table III) contains information on the first and last frequency to be used, the frequency increment, the quantity BOUND (which gives the frequency range within which lines are to be summed to obtain the attenuation at a fixed frequency), the choice of the spectral line profile to be used, and a choice of:

(a) summing over all the molecular constituents to get the total attenuation (zero in the sixth column), (b) just considering the

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TABLE II
Sample of Spectral Line Compilation

	FREO	STRENGTH	HALF HIDTH	ENERGY	DATE	ISO	CONSTITUENT
NO 0	F RECUR	05.	40				
140	•307	.151E-55	.1100	205 . 328	102		3
	•3+1	.199E-22	.1100	50.302	102		3
	.369	.199E-22	.1100	8.055	102		3
	1496	.183E-22	.1100	281 .833	102		3
	•539	.157E-22	.1100	345.692	102		3
	.742	121E-21	.0811	446.512	53		1
33	.756	.355E-22	.1100	171 - 501		666	3
	.856	·192E-22	.1100	127.264		666	3
	1966	·326E-22	.1100	301 4671		666	3
	1.002	.529E-22	.1100	128 - 119			3
	1.007	. 289F - 55	.1100	100.572		666	3
	1.018	.169E-22	.1100	157 - 147	102		3
	1.202	.395E-22	.1100	241.831		666	3
	1.262	·683E=22	.1100	156.903		666	3
	1.429	.254E-22	.1100	2.519	_	666	3
	1.456	.492E=22	.1100	77.082		666	3
	1 . 463	.110E-22	.1100	702.316		666	3
	1 . 4 9 7	.175E-22	.1100	190.212			3
	1.650	.578E=27	.0320	2460 . 774		66	7
	1.607	.171E-26	.0350	2230.425			7
	1.669	·318E-22	.1100	467.787	-	666	3
	1.676	.679E=24	.0900	155 - 389	52		
	1.604	.475E-26	.0350	2011 - 215			?
	1.701	125E-25	.0350	1803-180			7
	1.73	.515E-55	.1100	579 • 061			7
	1.718	.31UE-25	.0350	1606 - 353			3
	1.734	.575E-22	.1100	323.620			7
	1.735	•725E-25	.0320	1420 - 767			7
	1.753	.160E-24	.0320	1246 . 452			,
	1.764	.437E-27	.0320	1178-12			7
	1.7/0		.0350	1083 - 436			7
	1.773		.0350	1099 - 77			7
	1.781	.868E-27	.0320	1024 - 10			7
	1 . 7 8 8		.0320	931 • 74		200	7
	1.789		.0320	951 • 11:			3
	1.791		.1100	880.79			
	1 . 797		.0320	2339 • 13			
	1.800		.0380	791 • 40			
	1.806			813-16			7
	1.806		+0	2.3.10	ECHO!		
NO	OF RECO		.0380	748-21	9 75	5 68	7
	1.814		.0350	2211.58			
	1 - 819		.0370	685.95			
	1 . 8 2 3		.0350	662.43			
	1.824		.0350	626.38			
	1 . 831		.0370	2095 - 30	_		
	1 - 835			569.50			7
	1 . 8 4 0			544186		5 66	7
	1 . 8 4 2			281 - 83			3
	1 . 8 4 (

attenuation due to one particular molecular species (M in the sixth column), or (c) considering the attenuation due to all species except one (-M in the sixth column). The number in the seventh column chooses the caption to go with the atmospheric models described above. Three choices of line profile are currently available: Lorentz, Van Vleck-Weisskopf and Gross (kinetic). 7,8,9 These are denoted by 1,2, or 3 respectively in the fifth column. When the frequency at which the attenuation is being calculated coincides within .0005 cm with one of the spectral line frequencies in the data file, the three profiles mentioned have been replaced by a Voigt profile for the particular line for which this is true. In this case the center of the line is assumed to coincide exactly with the frequency at which the attenuation is being calculated and the Voigt profile at line center is used. This was found necessary because the vertical attenuation from a given high altitude out into space is greatly overestimated unless line broadening due to the Doppler effect is included. The Voigt profile includes a combination of collisional and Doppler broadening. The choice of Voigt profile at line center was made because this gives the maximum attenuation of which the line is capable. Any other frequency off line center will give a lower attenuation. SLAM program currently in use is shown in the Appendix.

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TABLE III

EXAMPLE OF CONTROL FILE

FREG.	FINAL FREQ.	FREQ. INTERVAL	BOUND	LINE	CON.	ATM.
2.040	2.040	-601	5•	1	7	6

II. METHODS OF CALCULATION

The atmospheric model directly gives the concentrations in grams per cubic meter for water vapor, Cl(N), and for ozone, C3(N), at the altitude represented by the (sequential) integer, N. These mass densities are converted into the number of molecules in a column 1 km long by 1 cm² crosssectional area, denoted by W(1,N) and W(3,N), repectively, by the formulae:*

$$W(1,N) = C1(N) * 3.346E+21$$

 $W(3,N) = C3(N) * 1.2546E+21$.

For those molecules, M, which have a constant mixing ratio, AM(M), the quantities W(M,N) are computed by the formula:

$$W(M,N) = (.724270E+24)*P(N)*AM(M)/T(N).$$

where the numerical factor is the reciprocal of k, the Boltzmann constant, times a power of 10. P(N) and T(N) are respectively, the pressure in millibars and the temperature in degrees Kelvin, as given by the atmospheric model. M=5 and 7 correspond to carbon monoxide and oxygen, respectively. The mixing ratio AM(M) represents the part of the atmosphere by volume that consists of the naturally occurring isotopic mixture of constituent M:

$$AM(5) = .075E-06$$

 $AM(7) = .2095$

^{*} $W(M,N) = CM(N)/(10*(Molecular Weight)*(1/12*M^{12}C)),$ M(12C) = mass of carbon-twelve atom.

Next, the population of each quantum state capable of absorbing energy in the spectral region under consideration must be determined. The fractional population is given by the expression

EXP(-E/kT)/Q(T),

the Boltzmann exponential population factor EXP(-E/kT) divided by the partition function Q(T), at the temperature T. In absorption, E is the energy of the lower state; k is Boltzmann's constant. The exponential population factor and the partition function have been evaluated at the standard temperature T0=296K and the results are included in the spectral line data file as a factor of the line strength. The corrections to these factors necessary at temperatures T other than TO are computed by the program. The exact quantum partition function was evaluated at TC=296K, 4-6 and the temperature correction is approximated by assuming the temperature dependency to be that of the classical rotational partition function (see e.g., Appendix D of Ref. 5). Thus, linear molecules are assumed to have a rotational function that varies directly as the temperature, and non-linear molecules one that varies as the 3/2-power of the temperature. The vibrational partition function at the standard temperature is included but its temperature dependence is neglected. The quantity necessary to adjust the exponential population factor from temperature TO to T(N) is

CSI(N) = (TO-T(N))/(TO*T(N)*.6946)

and the quantity necessary to adjust the partition function from TO to T(N) is given by

CS2(M,N) = TO/T(N)

HIAFKZINF KFZFVKCK INZIIINIF

for linear molecules, and by

$$CS2(M,N) = (T0/T(N)) ** 1.5$$

for non-linear molecules.

The stimulated emission at TO was included in the line strength on the original AFCRL data tape. However, the LBL program listed in Ref. (2) did not include corrections to the stimulated-emission factor at other temperatures. In the present SLAM program this stimulated-emission factor has been divided out of the line strengths in the data file and the SLAM program itself computes the required stimulated-emission factor at the arbitrary temperature T(N). This factor is

where GNU(I) is the wavenumber (cm⁻¹) of the spectral line whose contribution to the attenuation we are considering. The final value of the line strength, when multiplied by the exponential population factor and the stimulated emission factor, and then divided by the partition function is therefore:

Here S(I) is the line strength as it appears in the data file (DATA 2) and EPD(I) is the energy of the lower state from which the absorption arises. S(I) also includes as a factor the isotopic abundance ratios of molecules such as $0^{16}0^{18}$ which are included in the file.

Next, the line width must be calculated. The data file contains the half-width of the line at half-maximum at the standard temperature TO, and pressure PO = 1013 millibars. When the linewidth is assumed to be proportional to the pressure, the temperature and pressure dependence of the line

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width may be taken into account by calculating the factor:

$$CA(N) = ((TO/T(N))**0.5)*(P(N)/PO).$$

This factor, which is a first approximation, assumes that all lines of all species have the same temperature dependence as would occur when the collision diameters are independent of temperature. The half-width is therefore given by

$$ALPHA1 = ALPHA(I)*CA(N).$$

where ALPHA(I) is the half width at PO,TO of the Ith line given in the file.

Three line shapes can be chosen by the user for the calculations: the Lorentz, Van Vleck-Weisskopf (VVWF), and "kinetic" (Gross) line shapes. For any line shape, the auxiliary quantitities

$$Z = V-GNU(I)$$

are calculated first, where V is the wavenumber at which the attenuation is to be calculated, and GNU(I) is the wavenumber of the Ith line. If

the Voigt profile 10 is used for the calculation.

For the Lorentz line shape, the quantity

$$SUM1(M)=SS*ALPHA1/(Z**2+ALPHA1**2)$$

is calculated.

The Van Vleck-Weisskopf shape requires first the calculation of

$$VVWF = (1 \cdot /(Z**2+ALPHA1**2)) + (1 \cdot /(Z1**2+ALPHA1**2))$$

and then the calculation of

$$SUM1(M) = (SS*ALPHA1*(V**2)/(GNU(I)**2))*VVWF.$$

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The Gross (kinetic) line shape is obtained by first calculating the factor

and then calculating

SUM1 (M) =
$$SS*ALPHA1*4 \cdot *(GNU(I)**2)/GR$$
.

The Doppler broadening is determined by the parameter BETA which is the half-width divided by $\sqrt{\ln 2}$ of the Doppler broadened line at half-maximum. The quantities DOP(M) which depend on the masses of the individual molecular species M are stored in the program as DATA and are used to compute:

DOP1
$$(N1, N2) = DOP(N1) *T(N2) **.5$$

which now depends on the altitude and atmospheric model through dependence on the temperature T(N2). Then BETA is given by:

where the dependence on the line frequency is now included. The shape of the Voigt profile depends on the dimensionless variable Y:

which is the ratio of the Lorentz half-width to the Doppler parameter.

In the special case of the center of a line, calculation of the Voigt profile can be reduced to the calculation of the probability integral. When GNU(I)=30 cm⁻¹ and Z=.001 cm⁻¹ the parameters are already such that the Voigt profile can be approximated by a Lorentz shape. Therefore in the first approximation it was not thought necessary to replace the other profiles by a Voigt one except possibly for the line nearest the frequency at which the attenuation is being calculated. The expression to be evaluated is:

$$\frac{2}{\text{BETA}} e^{\mathbf{Y}^2 \int_{\mathbf{Y}}^{\infty} e^{-\mathbf{q}^2} d\mathbf{q}$$

where a factor $1/\pi$ has been omitted.

When (Y.GE.5.) the asymptotic formula for the probability integral is used, giving:

where Y3 is the third power of Y, etc. When Y is less than 5 an approximation of Hastings 11 is used. Let:

$$TY=1./(1.+.3275911*Y)$$

and TY3 be the third power of TY, etc. Then use of Hastings' approximation gives:

SUM1 (M) =SS*1.772454* (.2548296*TY

- .2844967*TY2+1.421414*TY3-1.453152*TY4

+1.061405*TY5)/BETA.

All line shapes given above neglect a possible shift of resonant frequency with pressure of about .01 cm⁻¹ per atmosphere. This sets a limit on the precision with which it is desirable to give the resonant wavenumbers in the data file. (Note that .001 cm⁻¹=30 MHz, a reasonable modulation bandwidth.) In addition, the exact shape of the spectral lines far from the resonant frequencies is not settled, especially for the case of water vapor. In this case, besides the usual monomer form, water dimers may exist and contribute appreciably to the absorption.

Currently, the continuum contributions (due primarily to $\rm N_2$ and in part to non-resonant absorption by $\rm O_2$) have not yet been included in the SLAM program. Thus, the attenuation in the vicinity of absorption minima will be somewhat underestimated.

To determine the attenuation, the quantities SUM1 (M) from the different lines of the species M must be added at a fixed wavenumber:

$$CAY1(M) = CAY1(M) + SUM1(M)$$
,

where this sum is iterated over all the relevant lines.

The quantity CAY1(M) is next multiplied by W(M,N) and the result summed over M:

CAY=CAY+CAY1(M)*W(M,N).

Finally, a normalization factor of $1/\pi$ omitted in the definition of the lineshape, and conversion of units into dB/km, gives the formula

OPD(IV)=CAY*1.38246

where OPD is the horizontal attenuation in dB/km.

In addition to the horizontal attenuations at the levels represented by N, the integrated attenuations from these levels down to the ground and up into space are calculated. The integration is performed by means of the trapezoidal rule. An iteration of the formula

SUM=SUM+.5*(H(N)-H(N-1))*(OPD(IV)+SAVE)

gives the attenuation from the height H(N) down to the ground level, where OPD(IV) is the horizontal attenuation at H(N), SAVE is the horizontal attenuation at the height H(N-1) and SUM is initialized to zero at the ground level. Then

DOWN (N, IV) = SUM

is the attenuation in dB from the level H(N) down to the ground,

HOR (N, IV) = OPD (IV)

is the horizontal attenuation in dB/km, while

UP(N, IV) = SUM-DOWN(N, IV)

In the latter formula SUM represents the attenuation from the highest level down to the ground. The wavenumber is then incremented and the calculation begun anew.

III. SLAM OUTPUT FORMATS

Typical output in tabular form is shown in Tables IV and V. Columns labeled HEIGHT give the altitude in kilometers above mean sea level, those marked HOR give the attenuation in the horizontal direction in dB/km, those marked DOWN give the total attenuation in dB from the height indicated down to sea level, while those marked UP give the total attenuation in dB from the height indicated vertically outwards into space. The numbers marked FREQUENCY give the frequency (in cm-1) at which the calculations were done. From the heading, we note that a Van Vleck-Weisskopf line profile was used in Table IV, that BOUND was 20 cm⁻¹, that all constituents on the data file were used in the calculation (shown by the value 0 after CONSTITUENT), and that the U.S. Standard Atmosphere, 1962 was used. This frequency is in a valley between two water vapor absorption lines. Table V shows the results of a calculation identical to that of Table IV, except that a Gross profile was used instead of the Van Vleck-Weisskopf profile. The two results for HOR differ by about 25% at sea level, but the difference grows considerably larger at high altitudes. At the peak of absorption lines little difference is found in the calculated attenuation as a function of line shape.

Figures 1 through 7 show typical graphical output. Figures 1 and 2 present graphs of HOR, DOWN and UP corresponding to the numerical output of Tables IV and V. The caption identifies the various curves and shows whether they are measured in dB or dB/km, i.e., whether the scale of ordinates on the left or on the right is to be used. The abscissa is the HEIGHT, and the caption gives information similar to that in the tabular output,

TABLE IV

SLAM Output for 7.200 and 7.300 cm⁻¹ with Van Vleck - Weisskopf Profile

V1- 7-8	7-200V2-	-300DV-		- TOUROUS	000				
	2.BOOVTOP	27.30	-	GNU(1)-	-10000 ·	27. 22.11	ATM 135	29	
7	3000 7-3	3280 VAN	VLE	CK-WEISSKOPF	PROF	TITUENT			
HEIGHT	4	27.00		•					
ć		200				201	230	5	
		•	J	130E	1.000	9202E 0	·+9132E	123	478
•		•	U	.49900E 00	.00	4437F O	101845		
3	796	•	.,	0		507126	1000	٠.	
000.9	*30472E=01	•	-	2046F=0		1 TO THE POPULATION OF THE POP	16034E	10364E	94E 0
000.8	417	•	•	30000		100035-0	ZPRZE		36
Q	4		, (116086	h .	901-1E-C	ZOE	-	3E-C
2.00	8086		,		-	19556-0	3013E		1E-0
0		•	9	BERGES	13.000	5			6E-0
	20-30-37-	•	0	-24808E-02	80	E-0	3080E		35-0
		061.	5	-34876E-02		. 61226E-03	3102E		
	00000		01	.24+88E-02	6	. +0477E=03	3112E	01 .17984F=C	45-0
Э (-3339E-03	.131	; 0	·1+305E-02	-	0	1119F		320E-02
	E0-3-0612.	161.	5	· 89264E=03	ë	. W	131235	1 70	DOODE
3	·133+3E=03	.131	01	.54836E-03		0-3	121246	7.3	014
000	26323E-0	·13129E	01	·10300E-03	35.000	2922E-0	121205		
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20.05	0-30g	313	010	O BOOOD	å	201295=0	• •		4 6
00	·53203E	130	01	0	•		300.00	000.	
DENCY	.300								
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000.	146E 0	300000	00	710F 01	. •	00 343976		•	
2.000	·24547E 00	8800	00	+8297F		17954E 0	47950	0	7E 00
00.	0-3+9+	-10984F				14431E	98319E	0	DE 00
0	0		• -	9		49366-01	11658E		DE 00
0	1775	7		,	000.	1/6/6E=01	2290E	-	0-36
10.000	**2671E=02	.12577F	• •	109515	000	64750E=02		1 -186836-01	36-01
2.00	216375			2	Ä (2613E	-1	3E-02
	1129*F=0	126715		201246646	91		•		11756E-02
6.00	61271F=0	34046	٠.	30330E-05	0		2681E	•	
8.00	3968	3000	;	20-14-05-05-05-05-05-05-05-05-05-05-05-05-05-	17.000	_	2464E	•	O
	191085				'n.	15E-03		•	16-03
2.00	104845	350/35	3 6	9	-	£246-03	2705E 0	•	0
0.4	364004			9	m	0150E-0+	2707E 0	1 .29850	0
	1	_	1	24888E-0	'n		708E 0	•	
	TOCOUR.	Z/09E		34147E-0	'n	2726E-05	2710E 0		
	DOIESE	3710E		9367E-0	45.000		2710E 0	1 .0000) C
	300//2	2710E	10	3000n	0	6704E=0	2710F 0		
		1							

TABLE V

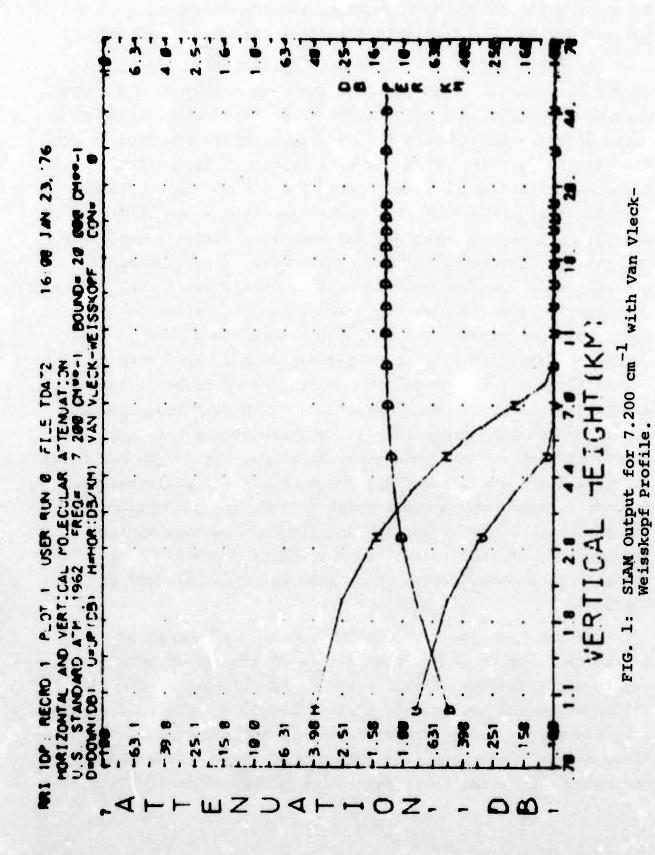
SLAM Output for 7.200 and 7.300 cm⁻¹ with Gross Profile

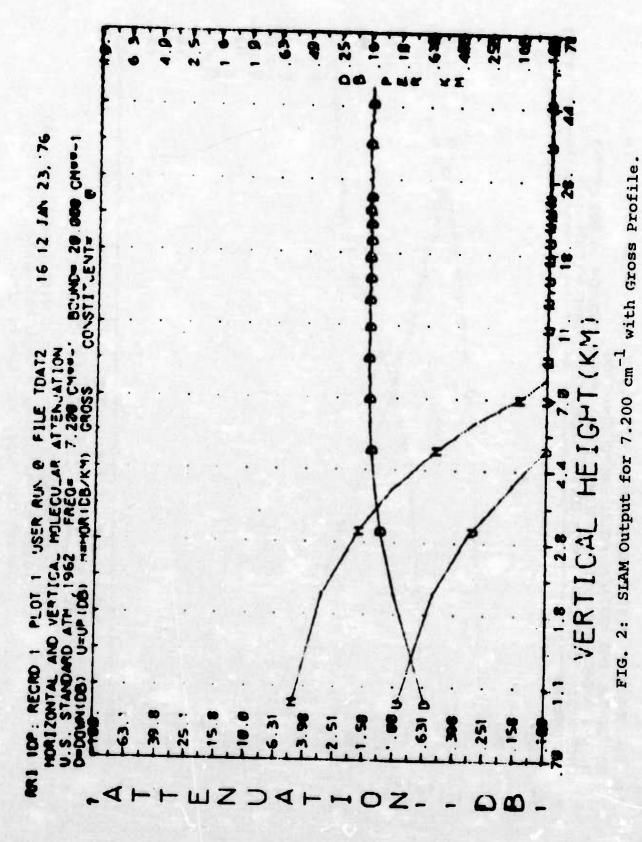
00P 27.3000NU(1)= 00 00NNU(1)= 00 00NNU(1)= 00 00NNU(1)= 00 00000E 00 1940DE 01 10000 5126EE 01 1526EE 01	V1= 7.8				TOOBOOM	20.00	9	ATH-1196	2
T. 3000 T. 3280 GROSS PROFILE CONSTITUENTS		V10	27.300	SNC	1)-	.3070K	27.328I	929	
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House Hous	REGUENCY	-20							
-0.00 -0.3546E 00 -0.0000E 00 -1.9476E 01 1.000 -1.7546E 00 -1.2495E 01 -1.30158E 00 -33077E 01 -1.3262E 01 -1.326	EIGH	ō	Z		1	HEIGHT	20	Z	5
	0	3564E 0	0000		19470E 0	1 100	48283E 0	60923E	.93772E
**************************************	.00	0701E 0	2400		8+280E 0	3.00	17540E 0	12+5+E	·30159E 0
8-000 11590E=02 1333E=01 7.000 1510E=01 3000 1500E=02 1530E=01 7978E 10-000 11590E=02 1333E=02 1333E=02 13.000 34570E=03 1547E=01 7978E 110-000 54506E=03 11494E=01 13913E=02 13.000 34570E=03 1547E=01 7978E 110-000 52737E=03 11496E=01 13137E=02 13.000 34570E=03 1547E=01 7978E 22-000 115914E=03 11496E=01 13137E=02 13.000 21473E=03 1547E=01 15213E=02 13.000 21477E=03 15496E=01 14913E=02 13.000 21497E=03 15496E=01 14969E=01 14969E=0	00.	8741E-0	13824		10452E 0	0 2.00	53066E-0	1+583E	-98618E-
12-000 - 155-00E - 157-15E 01 - 13715E 02 13-000 - 13039E 02 - 157-15E 01 - 127-15E 01 - 127-15E 01 - 127-15E 02 13-000 - 127-15E 03 - 157-15E 01 - 127-15E 02 13-000 - 127-15E 03 -	30	9180E-0	14995		4/496E=0	1 7.00	15108E-0	15216E	· 25352E
10.000	.00	1696E-0	5332		13715E-0	1 9.00	33039E-0	15390E	-79784E
12-000 0.5069E=03 15-34+E 11 -20139E=02 13-000 -3478E=03 -1544+E 11 -20139E=02 13-000 -3577E=03 -1545E 11 -1545E=02 13-000 -3277E=03 -1545E 11 -1545E 12-000 -3277E=03 -1545E 13 -3577E=03 -3545E 13 -3577E=03 -35	0.00	5540E=0	15414	01	55504E-0	2 11.00	94570E-0	15+27E	.43011
16.000 .22795E=03 .2549E	2.00	63069E-0	15434	01	35133E-0	2 13.00	46134E-0	15440E	-29678E-0
18.0.0	***	36737E-0	4	01	20539E-0	2 15.00	31478E-0	15447E	.22135
18.000	6.00	27276E-0	2	010	19197E=0	2 17.00	25777E-0	15+53E	·16546E
20.000 19514E=03 15465E 01 64375E=03 23.000 1175E=03 15465E 01 79727 22.000 1723E=04 15465E 01 64375E=03 23.000 17395E=03 15465E 01 321403 24.000 25413E=04 15465E 01 62105E=04 35.000 17395E=05 15465E 01 17166 40.000 10375E=05 15470E 01 201000E 00 70.000 50126E=05 15470E 01 00000 100.000 10375E=07 15470E 01 00000E 00 70.000 65996E=10 15470E 01 00000 100.000 10375E=07 15470E 01 00000E 00 70.000 65996E=10 15470E 01 00000 100.000 10375E=07 15470E 01 00000E 00 70.000 65996E=10 15470E 01 00000 100.000 103025E=07 15470E 01 14000E 01 1400E 01 14403E 01 15264 100.000 14612E=02 15245E 01 147706E=01 14703E=01 14703E 01 15264 100.000 14612E=02 15245E 01 14706E=01 14706E=03 15239E=01 14703E 100.000 14612E=02 15245E 01 14000E=02 11000 17334E=03 15239E=01 147036 120.000 14612E=02 15252E 01 140031E=02 11000 17332E=03 15239E=01 14703E 120.000 14612E=02 15252E 01 14741E=03 15000 1700E=04 15259E 01 17000 17000 120.000 14612E=02 15252E 01 140001E=03 15239E=04 15259E=01 17000 17000 120.000 14612E=03 15252E 01 140001E=03 15236E=03 15259E=04 15250E 01 17000 120.000 14612E=03 15252E 01 140001E=03 15250E=04 15250E 01 17000 120.000 14612E=03 15252E 01 140001E=03 15000 1700E=04 15250E 01 17000 120.000 14612E=03 15252E 01 140000E=03 15000 1700E=04 15250E 01 17000 120.000 14612E=03 15250E 01 140000E=03 15000 1700E=04 15250E 01 170000 120.000 17000E=04 15250E 01 17000 17000 17000 1700 170000 17000	8.00	3793E-0	4	010	1+076E-0	2 19.00	21553E-0	15+58E	.11816
22.000 14236E=03 15963E 01 64373E=03 23.000 11782E=03 15966E 01 51703 23.000 10372E=04 15966E 01 6473E=04 15969E 01 17166 10.000 10372E=04 15969E 01 184019E=04 15969E 01 17166 10.000 10372E=04 15970E 01 28610E=05 45.000 17799E=06 15970E 01 00000 10.2345E=07 15970E 01 00000 17334E 00 17334E 01	0.00	9514E=0	~	01	97656E-0	3 21.00	16473E-0	15462E	-79727E-
20.000 0.5513E=04 15465E 01 0.0001E=04 35.000 0.7661E=04 15466E 01 0.32234 32.000 0.0031E=04 15465E 01 0.0001E=04 35.000 0.50126E=05 15470E 01 0.0001E=04 35.000 0.50126E=05 15470E 01 0.0001E=04 15.000 0.0037E=07 0.0001E=04 15.000 0.0037E=07 0.0001E=07 0.00001E=07 0.00001E=07 0.00001E=0	2.00	4236E-0	~	01	0-36/6+9	3 23.00	11782E-0	15+6+E	-51+03
30.000 -20415E=04 -15450E 01 -80109E=04 -35.000 -50126E=05 -15450E 01 -17166	4.00	5133E-0	6.4	01	+0817E-0	3 25.00	76691E-0	15+66E	.32234E-
## ## ## ## ## ## ## ## ## ## ## ## ##	2000	3415E	.15469E	01	80109E-0	1 35.00	50126E-0	15469E	-17166E-
## ## ## ## ## ## ## ## ## ## ## ## ##	9	0372E-	~		28610E=0	5 45.00	17998E-0	15470E	-00000E
NOTICE 19470E 1	.00	24559E-0	15470		O BOOOD	0 10.00	5996E-1	5470	0000
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-000 -72656E 00 -00000E 00 -13261E 01 1.000 -47696E 00 -60177E 00 -92435 2-000 -30336E 00 -39194E 01 -14037E 00 3-000 -17334E 00 -12303E 01 -29883 4-000 -228829E=01 -14814E 01 -44708E=01 -14008E 01 -14008E 0	HOH	0	3		5	ш	~		<u>م</u>
2-000 -30336E 00 -39194E 00 -53418E 00 -17334E 00 -12303E 01 -29583 4-000 -97594E=01 -14814E 01 -14637E 00 5000 -14908E=01 -14408E 01 -22840 8-000 -28829E=01 -14814E 01 -14708E=01 7.000 -14908E=01 -15033E 01 -22840 8-000 -14612E=02 -15148E 01 -14368E=01 7.000 -32094E=02 -15204E 01 -57411 10-000 -14612E=02 -15245E 01 -14065E=02 11.000 -32094E=02 -15204E 01 -22841 12-000 -14612E=02 -15245E 01 -14065E=02 11.000 -17060E=03 -15249E 01 -723841 14-000 -13027E=03 -15252E 01 -34055E=03 15.000 -17060E=03 -15254E 01 -723841 18-000 -13027E=04 -15253E 01 -34052E=03 15.000 -17060E=03 -15254E 01 -18408 22-000 -22132E=04 -15256E 01 -14591E=03 23-000 -17706E=04 -15260E 01 -18408 22-000 -22137E=04 -15261E 01 -14591E=03 23-000 -17706E=04 -15260E 01 -18408 24-000 -22127E=06 -15261E 01 -00000E 00 -17706E=07 -15261E 01 -00000 50-000 -21271E=06 -15261E 01 -00000E 00 -17794E=07 -15261E 01 -00000 50-000 -21271E=06 -15261E 01 -00000E 00 -17794E=07 -15261E 01 -00000 50-000 -22278E=08 -15261E 01 -00000E 00 -17794E=07 -15261E 01 -00000	00.	72656E	00000		3192c	1 1.00	47698E 0	60177E	.92435
### ### ### ### ### ### ### ### ### ##	000	30336E	99194		53418E	9.00	17334E 0	12303E	·29583E
6.000 .28829E=01 .14814E 01 .44708E=01 7.000 .14908E=01 .15033E 01 .22840 8.000 .80407E=02 .15148E 01 .11364E=01 9.000 .32094E=02 .15204E 01 .57411 10.000 .14612E=02 .1527E 01 .34065E=02 11:000 .82660E=03 .15239E 01 .22631 14.000 .22483E=03 .15252E 01 .16031E=02 13:000 .17060E=03 .15249E 01 .72384 16.000 .22483E=03 .15252E 01 .92125E=03 17:000 .17060E=03 .15254E 01 .72384 16.000 .22483E=04 .15253E 01 .57411E=03 17:000 .10332E=03 .15254E 01 .72384 18.000 .82132E=04 .15253E 01 .53174E=03 21:000 .42990E=04 .15256E 01 .18406 22.000 .92193E=04 .15256E 01 .14591E=03 23:000 .17706E=04 .15256E 01 .15266 22.000 .44326E=05 .15261E 01 .10212E=04 35:000 .10174E=05 .15261E 01 .00000 20.000 .41326E=05 .15261E 01 .00000E 00 70:000 .41794E=07 .15261E 01 .00000	.00	97594E	13658		16037E	00.5	52446E-0	14408E	-85345E-
8.000	.00	28829E	1+81+		+4708E-	1 7.00	14908E-0	15033E	.22840E-0
10.000	000	80407E	5148		11366E-	1 9.00	32094E-0	15204E	•57411E=0
12.000 .49362E=03 .15245E 01 .10031E=02 .33.000 .32390E=03 .15249E 01 .11950 14.000 .22483E=03 .15252E 01 .92125E=03 17.000 .17060E=03 .15254E 01 .72384 16.000 .82132E=04 .15255E 01 .57411E=03 17.000 .10332E=03 .15257E 01 .72384 18.000 .82132E=04 .15253E 01 .53174E=03 19.000 .66237E=04 .15258E 01 .23174E=03 21.000 .42990E=04 .15258E 01 .14591E=03 21.000 .42990E=04 .15260E 01 .14591E=03 23.000 .7796E=04 .15260E 01 .14591E=03 23.000 .7796E=04 .15260E 01 .15260E 01 .15260E 01 .15260E 01 .15260E 01 .15261E 01 .00000E 00 .7796E=07 .15261E 01 .000000 00 .41794E=07 .15261E 01 .00000E 00 .70.000 .41794E=07 .15261E 01 .00000E 00 .41794E=10 .15261E 01 .000000 00 .41794E=10 .15261E 01 .00000000000 .41794E=10 .15261E 01 .000000000000000000000000000000000	0.00	14612E	5227		34065E-	2 11:00	\$2660E-0	15239E	.22631
14.000 .22483E=03 .15255E 01 .92125E=03 15.000 .17060E=03 .15254E 01 .72384E=18.000 .13027E=03 .15255E 01 .57411E=03 17.000 .10332E=03 .15255E 01 .5756E=18.000 .10332E=03 .15255E 01 .5756E=18.000 .53992E=04 .15255E 01 .23174E=03 21.000 .42990E=04 .15255E 01 .23174E=03 21.000 .42990E=04 .15255E 01 .14591E=03 23.000 .47994E=04 .15260E 01 .14591E=03 23.000 .27994E=04 .15260E 01 .14591E=03 23.000 .27994E=04 .15260E 01 .15260E 01 .15260E 01 .15396E=10 .15261E 01 .15261E 01 .15261E 01 .00000E 00 .47794E=07 .15261E 01 .28610E=04 .15261E 01 .00000E 00 .41794E=07 .15261E 01 .00000E 00 .41794E=07 .15261E 01 .00000E 00 .41794E=07 .15261E 01 .00000E	2.00	49362E	15245		10031E-	30.E: 2	32390E-0	15249E	-11950E-
16.000	4.00	22483E	15252		92126-	3 15.00	17060E=0	15254E	.72384E-
18.000 .82132E=04 .15258E 01 .39526E=03 19.000 .66237E=04 .15258E 01 .29182E=20.000 .53992E=04 .15259E 01 .23174E=03 21.000 .42990E=04 .15259E 01 .15406E=22.000 .37994E=04 .15260E 01 .14591E=03 23.000 .27994E=04 .15260E 01 .1539E=30.000 .27994E=04 .15260E 01 .1539E=30.000 .27994E=04 .15260E 01 .1539E=30.000 .27994E=04 .15260E 01 .1539E=30.000 .27994E=04 .15260E 01 .71526E=30.000 .271526E=04 .15261E 01 .15261E 01 .00000E 00 .41794E=07 .15261E 01 .00000E	6.00	13027E	15255		67411E	3 17.00	10332E-0	15257E	-+5776E-
20.000 .53992E=04 .15259E 01 .23174E=03 21.000 .42990E=04 .15259E 01 .15404E= 22.000 .34945E=04 .15260E 01 .14591E=03 23.000 .27994E=04 .15260E 01 .11539E= 30.000 .44326E=05 .15261E 01 .990599E=04 35.000 .10174E=05 .15261E 01 .71526E= 40.000 .21271E=04 .15261E 01 .00000E 00 70.000 .41794E=07 .15261E 01 .00000E 50.000 .76633E=08 .15261E 01 .00000E 00 70.000 .32278E=10 .15261E 01 .00000E	8.00	82132E	15258		30550E	19.00	66237E-0	15258E	-29182E-
22.000 .34945E=04 .15260E 01 .14591E=03 23.000 .27994E=04 .15260E 01 .11539E=24.000 .22193E=04 .15260E 01 .90599E=04 25.000 .17706E=04 .15260E 01 .71526E=30.000 .44326E=05 .15261E 01 .16212E=04 35.000 .10174E=05 .15261E 01 .28610E=40.000 .21271E=06 .15261E 01 .00000E 00 70.000 .41794E=07 .15261E 01 .00000E 00 70.000 .32278E=10 .15261E 01 .00000E 00 0.0000E	0.00	53992E	15259		23174E	3 21.00	42990E=0	15259E	-18406E-
24.000 .22193E=04 .15260E 01 .90599E=04 25.000 .17706E=04 .15260E 01 .71526E=30.000 .44326E=05 .15261E 01 .16212E=04 35.000 .10174E=05 .15261E 01 .28610E=40.000 .21271E=06 .15261E 01 .00000E 00 45.000 .41794E=07 .15261E 01 .00000E 00 50.000 .32278E=10 .15261E 01 .00000E 00 0.0000E=00 .15261E 01 .00000E	2.00	3+9+5E-0	15260		14591E	3 23.00	27994E-0	15260E	-11539E-
30.000 .44326E=05 .15261E 01 .10212E=04 35.000 .10174E=05 .15261E 01 .28610E=40.000 .21271E=06 .15261E 01 .00000E 00 45.000 .41794E=07 .15261E 01 .00000E 00 50.000 .32278E=10 .15261E 01 .00000E 00 0.000 .32278E=10 .15261E 01 .00000E 00 00.000 .32278E=10 .15261E 01 .00000E	4.00	22193E=0	260		90599E-	4 25.00	17706E-0	15260E	.71526E-
40.000 .21271E=06 .15261E 01 .00000E 00	00.0	++356E-	261		16212E-	4 35.00	10174E-0	15261E	·28610E
\$0.000 .76633E=08 .15261E 01 .00000E 00 70.000 .32278E=10 .15261E 01 .00000000.000 .89594E=15 .15261E 01 .00000E 00	0.00	21271E-	5261	01	BOE	00.54	41794E-0	15261E	-00000E
00.000 .89594E=15 .15261E 01 .00000E 0	0.00	76633E-	15261	010	DOODE	00.07 0	2278E-1	15261E	0000
	00.00	9594E-	5261		3000n				

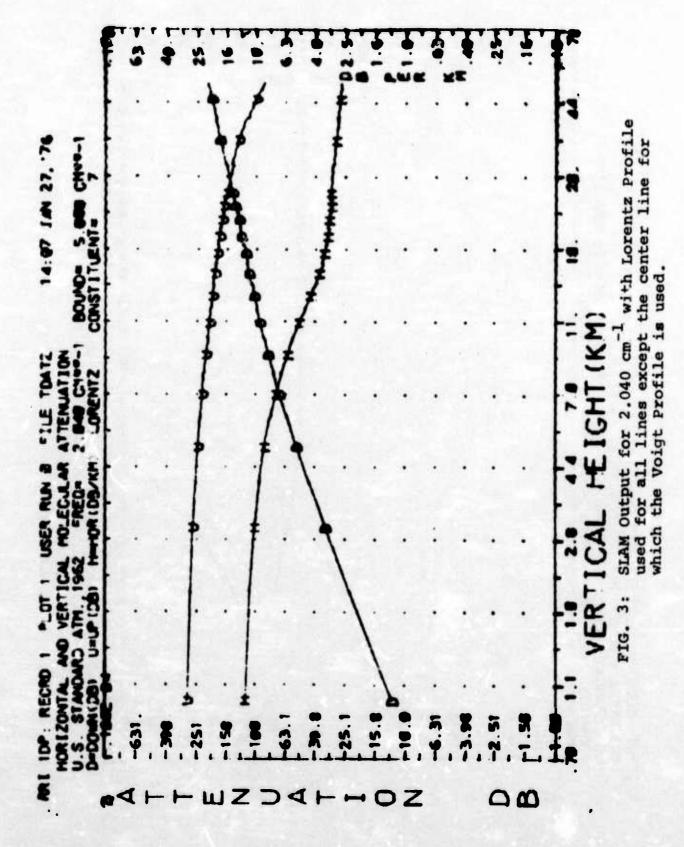
concerning the choice of parameters for the calculation. Comparison of Fig. 1 and 2 again shows the effect of line shape.

Figures 3 and 4 plot the computed attenuation for a frequency of 2.040 cm⁻¹, which is at the peak of the 60 GHz oxygen microwave absorption band. Figure 3 shows the attenuation computed as described above with the Voigt profile substituted for the Lorentz profile for the nearest line. In Figure 4 the Lorentz profile at the center of a line has been used for this line too. Corresponding numerical values are shown in Tables VI and VII. It can be seen that HOR begins to differ appreciably for the two cases above 50 km. This lends to a considerable difference in the computed value of UP at all altitudes. Although the Lorentz line shape was used for this calculation in order to facilitate comparison with the work of Liebe and Welch, 13 the Van Vleck-Weisskopf profile is generally considered more accurate in the microwave region and the Gross profile is perferred in the submillimeter region. Comparison of Fig. 3 with Fig. 1 or 2 shows considerable difference in the shape of the altitudedependent curves. The relatively fast drop-off of the HOR curve in Figs. 1 and 2 is undoubtedly due to the small scale-height for water vapor, which contributes most of the absorption in the troughs. The scale-height for oxygen, however, is the same as that of the atmosphere as a whole, so that HOR at the peak of an oxygen absorption line does not fall off as rapidly.

Figures 5, 6, and 7 are calculated at a frequency of 14.169 cm⁻¹, which is the peak of one of the strong molecular oxygen submillimeter lines. Figure 5 is calculated with all the constituents in the data file (CONSTITUENT =0), Fig. 6 with only the oxygen lines (CONSTITUENT =7), and Fig. 7 with all lines except those of oxygen (CONSTITUENT =-7). Otherwise, the calculations for these figures were done using identical







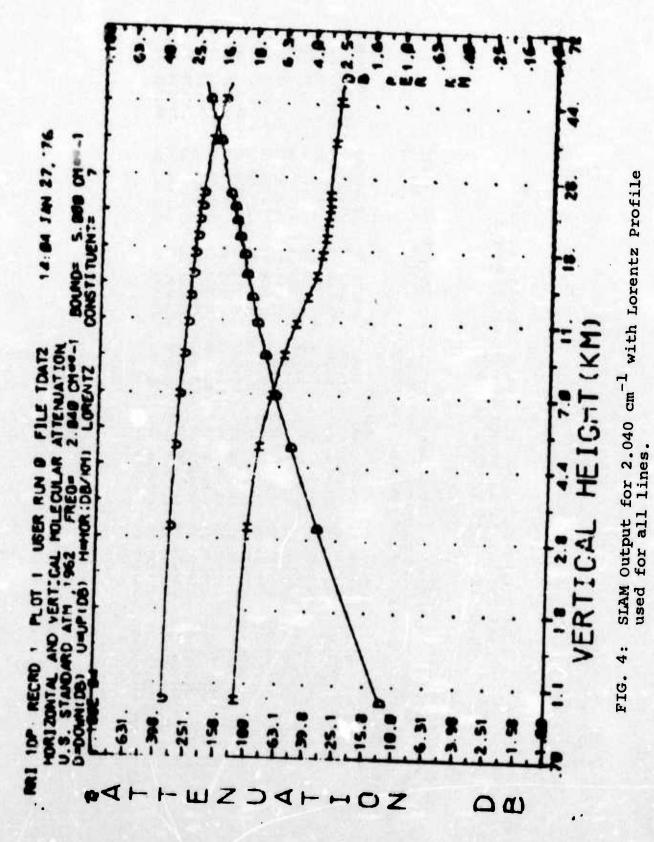


TABLE VI

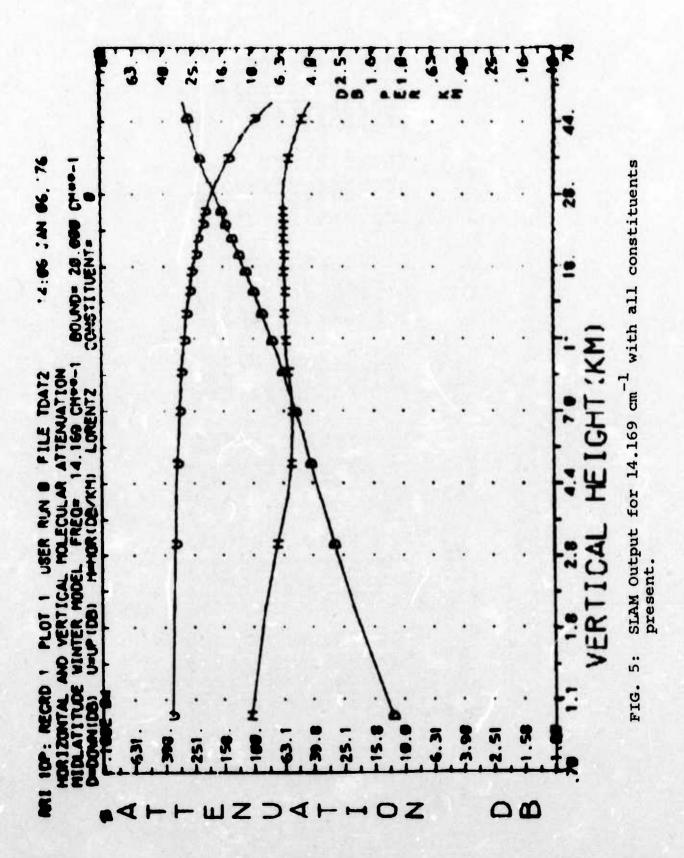
SLAM Output for 2.040 cm⁻¹ with Lorentz Profile used for all lines except the center line for which the Voigt Profile is used.

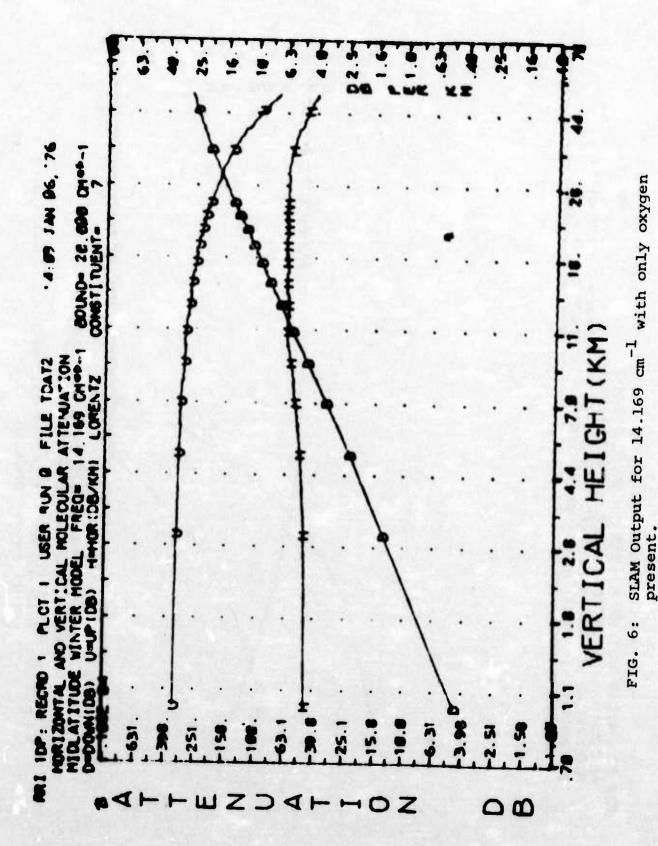
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		-	87/8	26598E	24724E	23141E	-21819E	20709E	97815	SOROF	19745	1000	700	3E960	6335E	\$718F	1	C/CSE	9348E	36360F
.9				_	020	020	02	02	60						_ 00	EO	0 0			60
ATM 196			16000E	33003E	2002	-	-	92753E	10203E	10895E	11708F	4466	11.000	13061	13649E	1+266E		3000	0033E	26348E
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STANDARD 7.17011		785	J L	1 4	1 6		1.1	لما	SIE O	DZE 0	141	1 40				OE O	4.		J	3E 0
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5.000 U .3070NU= CONSTITUENT=	DH7	1.000	C		•	0000	9.000	-	13.000	15.000	17.000	19.000	•		ָ י י	25.000	35.000	0		00000
	HEIGHT	. E0	50	E 0		2 (700	7	E .		60	60	E		,	7	9	(7)	•	v
11:63 •100BOUND= (1)= PROFILE	7	·29984E	1	36236	38985		1010101 1010101		-2023E	w	w	•17938E C		1 14	14001	102001	•1+203E 0	•11309E 0	43.64	3070
O+OGNU ORENTZ		00	02	02		1 0	ם סכ				60	60	60	60		ים ס	60	60	00	
200	DCWN	-00000E	.23348E	-+3609E	-60864F	-78344E		ı Q	-2/610E	. TOPICE	•11359E	•12047E	•12702E	•13337E	129895	000	5781	·18675E	PISE 15.	
.17		05	02	01	01	0			1	3 6	10	: O		01	0.1		5	10	0.1	
Z • 0 + 0 0 2 2 • 0 + 0 0 0 2 2 • 0 + 0 0 2 2 4 0 0 2 2 4 0 0 2 2 4 0 0 0 4 0 0 0 4 0 0 0 4 0 0 0 4 0 0 0 0 4 0	HOR	N	(7)	· 53650E	-79036E		· 55315F		364496			BOSEES.		·31373E			163734 1		·26062E	1
, v ,	HEIGHT	0000	8.000	000-+	0000.9	8.000	10.000	12.000	000			2000	20.00	55.000	24.000	20.00		00000	50.000	00000

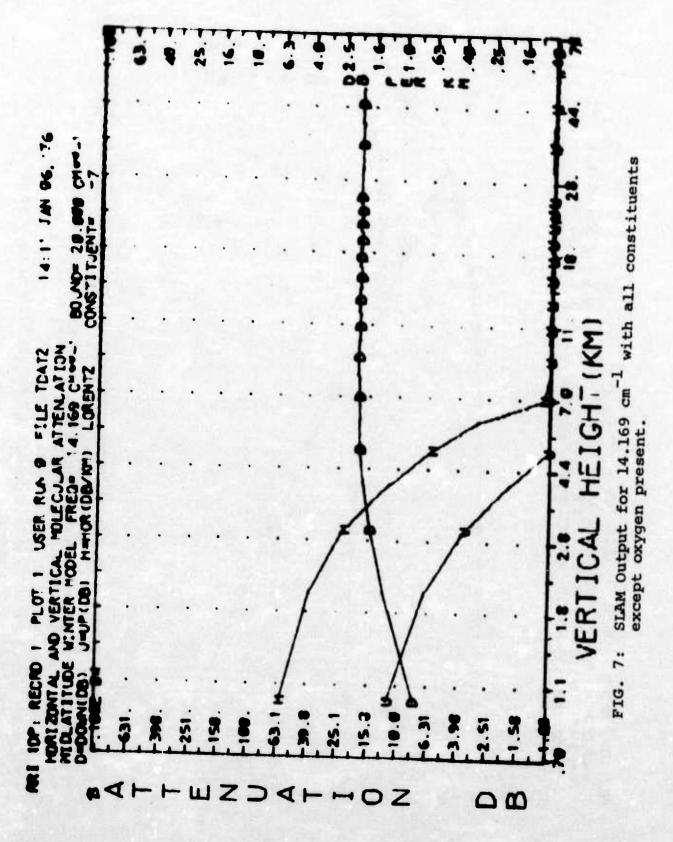
TABLE VII

SLAM Output for 2.040 cm⁻¹ with Lorentz Profile used for all lines.

**	040V2-		2.040DV=	7.040avir 11	.100BOUND-	-0	5.000	U.S. STA	STANDARD	ATR	1962		
8.0400	*0	2-1700		ENTZ	PROFILE		CONSTITUENT		17011	227			
SOI			Dawn		•	1	+10+1						
112	44.25	00	-50000	0	- 2000	•		X OF	ZZOO	Z		20	
				•	3+0505.	2	1.000	•11675E	0	.120KEF	0	- 3800	
:	TOROT	20		05	-33970F	03	00000				•	Bener.	
0	-93650E	0	190954.	0.0	191019	• •	•	300101	V O	-33863E	0	.32918	
-	790365	01		0 0	300000	•	•	-86204E	5	.52602E	07	.31044	
		: :		u O	301705.	•	2.000	•72265E	01	·68429F	C	. 29444	
•	3596C0.	5	./5341	20	.28770F	a	0000	40000			•		
60	·55315E	50	.87438E	0	2784.0		•	3+1500.	5	.81656E	05	.28139	
	1641491				3100.3	3	11.000	38660g·	6	·92753E	0	.2703	
	1	: :		70	354207.	0	13.000	• +2331E	01	102035	C		
	354736	5	.10612	ر	.25692F	EO	18.000	327975			•		2
m	35543E	01	.11389F	0	24048	• •		-3/606E	5	10995E	m 0	.25309	
	5			3 6	36454	2	17.000	34308E	50	11708E	0	.24894F	
	1000	::	3/10	20	228	EO	19.000	·32711E	01	2377	0		-
all.	366035	5	320/21.	60	-23603E	E0	21.000	-31740E		1000			
20	2	6	·13337E	60	-22947E					13061F	7	. 23283	ā
L.	304805	01	.139ROF			0 0	3	308015.	010	13649E	60	.226555	C
	П		30000	200	304697.	2	25.000	-304 + OE	01	14246	C	. 2203	•
u	7	010	·15781E	60	· 205235	03						300033.	60
N	27794E	5	.1847RE	0	7498		D (3/0063.		17255E	03	· 19049E	Q
0	c	:	-	3	3636/7.	2	42.000	·26651E	C1	200365	60	307671.	
u	?	;	396613.	m O	-1+6+8	E 0	70.000	T-CACC.		3000		2000	
m	1394E	010	-36304E	60	-00000	0	•	310000		SYNSOE	m	· 92842E	0
)							







values of the parameters. Comparison of Figs. 5 and 6 shows that the general altitude-dependence of the attenuation can be traced to the oxygen. Figure 7 shows that the other constituents make an appreciable contribution at low altitudes. Thus, the importance of including the oxygen submillimeter spectrum in this spectral region is illustrated.

IV. COMPARISON WITH CALCULATIONS BY OTHERS

Table VIII shows the results of varying BOUND within the SLAM program for a frequency of 1.000 cm⁻¹. Also shown are a comparison with calculations by Van Vleck. In these calculations only lines in the spectrum of water vapor are taken into account, all line half-widths are put equal to .1 cm⁻¹ and the temperature and pressure shown in the table are used instead of one of the standard atmospheric models. This was done to make a closer comparison with Van Vleck's results. The quantity given in the table is the horizontal attenuation in dB/km per unit density of water vapor, the latter expressed in g/m³. The results agree to about 3.6% which is considered satisfactory.

Table IX shows a comparison of the results of calculations performed by SLAM with those performed at AFCRL⁴. The results of varying BOUND within the SLAM program for this higher frequency are also shown. The discrepency between the SLAM and AFCRL calculations is about ten percent. This is considered a reasonable agreement; further comments are difficult to make since full documentation concerning the AFCRL calculations are not available at RRI.

Table X compares the results of SLAM and those of Liebe and Welch 13, using the Lorentz profile and U.S. Standard Atmosphere, 1962 used by those investigators. The quantities BOUND and CONSTITUENT are set so that only the oxygen microwave spectrum contributes to the attenuation. The discrepancy between the two calculations ranges up to a factor of two at 10 km. It is believed that this discrepancy can be traced to different assumptions made concerning the variation of line half-width

_ e					
CONSTITUENT = 1 PRESSURE = 1013 mb	140.	0.00602 0.00603 0.00603 BOUND		4.	14 COMPARISON BETWEEN SLAM PREDICTIONS AND VAN VLECK PREDICTIONS
S E	120.	0.00			A A
	2	ND 02			VLE
ROFILE	<u>00</u>	0.006 N BOU	TOTAL 0. 00603	0.00586	D VAN
PF P		595 S 0	L' 0	0	A
SSKO	.08	0.00 TION			IONS
WEIS)589 REDIC	0. 00116	9110	DICT
- - - - -		0.00 PR	0.00116	0.00116	PRE
VAN VLECK - WEISSKOPF PROFILE		0.00487 0.0054I 0.00575 0.00589 0.00595 0.00602 DEPENDENCE OF SLAM PREDICTIONS ON BOUND			SLAM
	8	CE C	line	11	WEEN
). 0054I ENDEN	1. 35 cm ⁻¹ line 0. 00487	0.0047	N BET
_ T	20.	7 0 DEP			1501
cm = .10	45	0048			1P AR
1.000 1.000 1.000	0		~	g/m ³	80
FREQUENCY = 1.000 cn LINE HALF-WIDTH = . TEMPERATURE = 293 K	Cm ⁻ l	III III	db/km g/m ³	×	
UEN(HAI	9	9 5	9	VLEC	
FREQUENCY = 1.000 cm ⁻¹ LINE HALF-WIDTH = .1 cm ⁻¹ TEMPERATURE = 293 K	BOUND (cm ⁻¹) 0.45	HOR (db/km) g/m ³	SLAM (db/km)	VAN VLECK (db/km)	
т-2/306-3-1	14				

TABLE VIII

0.04

0.037

0.037

0.037

0.032

MIDLATITUDE WINTER MODEL	AFCRL (dB/km)	27.4
FILE		100 25.28
OPF PRO	-1 -	75 25.26
AN VLECK-WEISSKOPF PROFILE CONSTITUENT = 0	SLAM (dB/km)	<u>50</u> 24, 94
VAN VLECI		$\frac{1}{2} = \frac{20}{23.64}$
29. 713 cm ⁻¹		BOUND(cm $^{-1}$) = 20.
FREQUENCY = 29.713 cm ⁻¹	HEI GHT (km)	• 0

* HORIZONTAL ATTENUATION

ATTENUATION BETWEEN THE GIVEN LEVELS

TABLE IX

COMPARISON OF SLAM RESULTS WITH AFCRL RESULTS

RIVERSIDE	RESEARCH	INSTITUTE
-----------	----------	-----------

U. S. STANDARD ATMOSPHERE	CONSTITUENT = 7 (1962)	HOR	(LIEBE AND WELCH ¹³) (dB/km)	14.4	10, 85	5.4	2 75
LORENTZ PROFILE		HORIZONTAL ATTENUATION (SLAM)	(dB/km)	12. 45	5.55	3.20	2.51
FREQUENCY = 2.040 cm ⁻¹	BOUND = 5	HEIGHT	(km)	0	01	20	30

COMPARISON BETWEEN SLAM AND LIEBE AND WELCH

TABLE X

MIAFKZINF HEZFWARM INZIIINIF

with altitude. The SLAM program assumes line half-widths characteristic of well separated, isolated lines, which is justified for low pressures of the broadening gas. However, due to interaction between overlapping lines, at higher pressures the attenuation far from the oxygen band is overestimated by this procedure. An empirical correction is often made by decreasing the assumed line half-widths until the calculated attenuation outside the band matches the observed result. In the calculations of Liebe and Welch this empirically corrected line half-width has been used up to an altitude of about 15 km after which a gradual transition to the line half-widths characteristic of the isolated lines is made. Since at 10 km the overlapping of the lines has decreased considerably this could account for the large discrepancy between the two calculations at that altitude.

V. COMPARISON WITH EXPERIMENTS

Table XI shows a comparison of SLAM output with experimental results of Becker and Autler 15 and of Burroughs, Jones and Gebbie 16. Only attenuation by water vapor is included and the results are normalized to 1 g/m of water vapor. Again, instead of one of the standard atmospheric models, the temperature and pressures shown, appropriate for a comparison with the corresponding experiment, have been used. There is substantial agreement between experiment and the results of either the Van Vleck-Weisskopf or Gross profiles at .784 cm⁻¹, which is near the 22 GHz water vapor absorption line. Further from this line the discrepancy increases to a factor of about 50% at 1.160 cm⁻¹ and 100% at 1.340 cm⁻¹. The Lorentz profile results are considerably more discordant. The values quoted from Burroughs, Jones and Gebbie have been obtained by evaluating their least squares fitted polynomial, which is a function of the broadener pressure, at the appropriate value of the atmospheric pressure. In this evaluation the term independent of the broadener pressure has been omitted as being due to the broadening of the water vapor lines by water vapor, which is not included in the SLAM program. It can be seen that the experimentally determined attenuations are still considerably higher than the calculated ones.

Table XII compares the SLAM output with atmospheric observations by Lo, Fannin and Straiton 17. These numbers have been taken from one of their fitted curves. Also shown are the decomposition of the calculated absorption into the sum of absorption by oxygen and by water vapor. From the above discussions it follows that two compensating errors are present in these

PRECEID
BOUNC = 100 cm ⁻¹
CONSTITUENT = 1

PRESSURE = 1 ATM		EXPERIMEN	0.023015	0.006715	0.008615	11.516	48.216	
PRESSUR		GROSS	0.0224	0.00406	0.00441	7.03	39.9	
BOUNE = 100 cm ⁻¹	HOR dk/km q/m³	VAN VLECK WEISSKOPF	0.0240	0.00371	0.00345	6.54	38.58	
8		LORENTZ	0.8498	0, 8438	0.8502	6.00	42.77	
CONSTITUENT = 1	TEMPERATURE (^O K)		318	(L)	318	293	293	
SNO) -34-	FREQUENCY (cm ⁻¹)		0. 784	1. 160	1.340	29.713	32. 166	

COMPARISON OF SLAM OUTPUT WITH SOME EXPERIMENTS

TABLE XI

		SNO	RIV	ERSIDE	RESEA	IRCH IA	ISTITUT	TE .
BOUND = 100cm ⁻¹		OBSERVATIONS			0. 16 ¹⁷			0.52 ¹⁷
BOUND		GROSS	0.0538	0. 196	0.25	0.306	0. 292	0.598
	UP (dB)	VV-W PROFILE	0.0456	0. 132	0. 18	0. 167	0. 488	99 0
RD ATM., 1962		LORENTZ PROFILE	11. 48	0.359	11.84	12.71	0.210	12.92
U. S. STANDAR	NOO		1	7	0	-	7	0
	FREQUENCY	(cm_t)	1. 167	1. 167	1. 167	3.160	3.160	3, 160

COMPARISON OF SLAM OUTPUT WITH SOME OBSERVATIONS

TABLE XII

calculations. The excess attenuation by water vapor is not included in SLAM, while the attenuation due to oxygen is overestimated due to neglect of the interacting line mechanism. Once again the Lorentz profile results are very large. Table XIII shows the considerable variation of the Lorentz profile results with BOUND. These results can be attributed to the large low frequency tail from the Lorentz profile of lines at high frequencies.

9.864

8 8

	CONSTITUENT = 0	UP (dB)	0.260	0.260	0.314	1. 795	4.80
LORENTZ PROFILE	U.S. STANDARD ATM., 1962	HOR (dB/km)	0.0706	0.0706	0.0977	0. 803	2.26
	FREQUENCY = 3.160 cm ⁻¹	BOUND	5.	7.	10.	20.	40.

VARIATION OF ATTENUATION WITH BOUND

TABLE XIII

VI. FURTHER REFINEMENTS REQUIRED

Several items which were not yet included in the program and which might have an appreciable effect on the attenuation are discussed below. In the SLAM program so far, we have neglected the continuum attenuation of nitrogen. Using the data of Gebbie, et. al. 18 we estimate the horizontal attenuation due to this cause at ground level to be about 1.5 dB/km at a frequency of 100 cm⁻¹, the peak of the nitrogen continuum absorption curve, and 0.2 dB/km at a frequency of 35 cm⁻¹. The nitrogen continuum should be included, but it is not likely to change the general shape of the attenuation curves. Several trace species having active rotational spectra are present in the stratosphere, and it is desirable to estimate the strengths of their absorption lines. These include nitrous oxide, nitric acid vapor, nitrogen dioxide, sulfur dioxide, and nitric oxide. 19

A low-altitude effect that should be dealt with is the excess attenuation of water, beyond that calculated from the individual lines of the water monomer. This is especially noticeable in the troughs between the peaks of the water monomer absorption. This excess absorption can have three causes. The line profiles of the water monomer may be different from that assumed, leading to greater absorption in the wings of the lines, and hence in the troughs. Water dimers 20-23 can contribute their own spectrum of absorption, and lastly, short-lived collision complexes of the water molecule with the broadening molecule may induce a temporary electric dipole moment, leading to increased absorption. These three possible causes can be largely separated from each other by considering how they scale with the physical variables of the problem: water-vapor pressure, pressure of the external broadening gas, and temperature.

Various cases can be distinguished: If S is the integrated strength of a line and α its half-width at half-maximum, then at the center of an isolated line, the attenuation is proportional to S/α ; in the wings, it is proportional to $S \alpha$; and for a group of lines with strength S that overlap due to the collisional broadening, it is S. For water monomers, S is proportional to the partial pressure of the water vapor; for dimers, it is proportional to the square of the partial pressure, and for collision complexes of water molecules with nitrogen, it is proportional to the product of the partial pressures of water vapor and nitrogen. Likewise, the quantity α is proportional to the partial pressures of nitrogen and water vapor for broadening by nitrogen and water vapor, respectively. For collisionally induced absorption, α is independent of any of the pressures. From the data of Burroughs, Jones, and Gebbie, 16 taken at 311 and 337 µm in pure water vapor, the attenuation is proportional to the square of the water vapor pressure. From the above scaling laws, this might be due either to attenuation from the wings of well-separated monomer lines or to overlapping dimer lines. However, the rapid change of attenuation with temperature was interpreted by these experimenters as evidence of water dimers.

At altitudes higher than about 40 km, Doppler broadening will be important. Its neglect imparts a spuriously large value to the attenuation at a line center at high altitudes because the attenuation at a line center varies inversely with the line width when Doppler broadening is neglected, while the pressure-broadened line width narrows with increasing altitude. The effect of the decrease in line width with altitude will tend to counterbalance the decreasing concentration, leaving a tendency to a spuriously constant attenuation at the center of a line. This effect has been allowed for in the SLAM program as described above. However the effect of Doppler broadening on the wings of the lines is not yet included. This would involve

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combining the Doppler broadening with collisional broadening not only when the latter is described by the Lorentz profile but also when it is described by the Van Vleck-Weisskopf or Gross profiles. Another high-altitude effect that must be considered is Zeeman splitting of the oxygen lines.

At lower altitudes, the profile of two overlapping lines of a single molecular constituent is not necessarily equal to the sum of the profiles of the individual lines (as assumed in SLAM). This consideration is particularly important for the microwave spectrum of oxygen. Recent results suggest how this can be taken into account in the future.

Finally, we note the influence of the method of integration upon the computed vertical attenuations. A rough calculation in one particular case showed an 8% difference between the results of the trapezoidal-rule integration and a higher-order method.

ACKNOWLEDGEMENTS

The author wishes to acknowledge helpful discussions with, and suggestions from, M. Greenebaum of RRI, who also carefully reviewed the manuscript. S. Rosenberg of RRI helped with aspects of the computer programming. Acknowledgement is also due for the free use that has been made of data tapes and programs supplied by R.A. McClatchey of AFCRL.

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APPENDIX

SLAM Program Listing

```
0030:
           OK,00306314
                          01/13/76
                                      13147
        OIMENSION H(7,33), GNU(3000),8(3000),ALPHA(3000),EOP(3000)
        DIMENSION MOL(3000), CAY1(7), FNU(100)
        DIMENSION SUM1(7), BINBUF(4,40), IBINBUF(3,40)
        DIMENSION H(33), P(33), T(33), C1(33), C3(33)
        OIMENSION CS1(33), C82(7,33), CA(33), AM(7), OOP(7), OOP1(7,33)
        DIMENSION DDWN(33,100), HOR(31,100), UP(33,100)
        AM(M) REPRESENTS THE PART OF THE ATMOSPHERE BY VOLUME THAT CONSISTS
        DATA AM(2),AM(4),AM(5),AM(6),AM(7)/33D.E-06,.28E-06,.075E-06,1.6
       ZE-06,2.095E-01/
        THE FOLLOWING PARAMETERS DEPEND ON THE MASS OF THE INDIVIOUAL
        MOLECULES AND DETERMINE THE DOPPLER BHOADENING
        DATA 00P(1),D0P(2),U0P(3),D0P(4),00P(8),00P(6),00P(7)/
       21.013850E-7,4.484607E-8,6.208538E-8,6.484607E-8,8.128885E-8,
       31.075350E-7,7.603875E-8/
       THE NEXT DATA REPRESENT THE CAPTIONS FOR THE VARIOUS
        ATHOSPHERIC MODELS
        INTEGER MODEL (7,6)/
      Z'MIOLATITUDE WINTER MODEL
               TROPICAL MODEL
                                   .,
      4 MIOLATITUDE SUMMER MODEL
                                    1,
      S'SUBARTIC WINTER MODEL
                                    ٠,
      6'BUBARTIC SUMMER MODEL
      7'U.S. STANDARO ATM. 1942
       PI=3-14159
       IV-1
       THE ATMOSPHERIC MODEL IS READ! HEIGHT IN KM, PRESSURE IN MS, TEMPERAT-
       URE IN DEGREES KELVIN, WATER VAPOR AND DZONE CONTENT IN G/(M443)
       READ(1)77)(H(I),P(I),T(I),C1(I),G3(I),I=1,33)
   77 FORMAT(F10.3,E10.4,F10.3,2E10.4)
       W(M)N) IS THE NUMBER OF MOLECULES OF SPECIES M AT A HEIGHT REPRES-
       ENTED BY N THAT IS CONTAINED IN A COLUMN OF ATMOSPHERE 1 KM IN
      LENGTH AND 1 CHOOS IN CROSS SECTIONAL AREA
      00 7 M=1,7
      00 7 N=1,33
    7 H(MJN)=(+724270E+24)+P(N)+AM(M)/T(N)
      00 8 N=1,33
      W(1,N)=C1(N)+3.346E+21
    8 W(3,N)=C3(N)+1+25+6E+21
      CHOICE OF PARAMETERS FOR THE CALGULATION ARE READIINITIAL AND FINAL
C
      FREQUENCY, FREQUENCY INCREMENT, RANGE OF FREQUENCY FOR WHICH LINES
C
      ARE SUMMED, SHAPE OF LINE PROFILE, CONSTITUENT, AND CAPTION FOR
      ATMOSPHERIC MODEL
      READ(3,85)V1,V2,DV,BOUNO,LP,IC,MOO
   85 FORMAT(4F10-3,315)
     LP1-LP
      HRITE(111,87) V1, V2, DV, BOUNO, (MOOEL (KK, MOO), KK=1,7)
  87 FORMAT('V1=',F10.3,'V2=',F10.3,'PV=',F10.3,'8DUND=',F10.3,2X,6A4
     VBCT=V1=BOUND
     VTUP=V2+30UND
     I=1
     ILL=1
```

```
DATA ON BPECTRAL LINES ARE READ FROM A BINARY FILE
    1 READ(2) IREC, ((BINBUF(JJ,K),JJ=1,4), (ISINBUF(JJ,K),JJ=1,3)
     ZAKelAIREC)
      OPTIONAL STATEMENT FOR GOING CALCULATION IN DOUBLE PRECISION
C
    1 CALL READDP(IREC, SINBUF, IBINBUF)
      TMAX-BINBUF (1) IREC)
      IF (TMAX.LT. VBOT) GO TO 1
      DO 9 KOLA IREC
      GNU(I)=BINBUF(1,K);5(I)=BINBUF(2,K);ALPHA(I)=BINBUF(3,K);
     REOD(I)-BINBUP(4,K))MDL(I)-IBINBUP(2,K)
       IF (QNU(I) .LT . VBDT) QD TO 9
       IF (QNU(I) . QT . VTOP) QD TD 11
       I=I+1
    9 CONTINUE
      IF(I.GT.2960) I=I=1160 TO 11
       00 TO 1
   11 I1-I
       WRITE(111,97) VBOT, VTOP, GNU(1), GNU(11), I1
   97 FORMAT('VBOT', F12.3, 'VTOP', F12.3, 'GNU(1)=', F12.3, 'GNU=', F12.3, 'Il'
     LAILS
       ISel
       V2P-GNU(II)-BOUNG
       IB-1
       P0-1013-00
       TO-296.00
       CB1(N) AND CB2(M,N) ARE FACTORS NECESSARY FOR THE CALCULATION OF
THE POPULATION FACTOR AND THE ROTATIONAL PARTITION FUNCTION AT
CC
       TINI, RELATIVE TO 290 DEGREES KELVIN
C
       DO 2 No1,33
    2 CB1(N)=(TO=T(N))/(TO+T(N)+.6946)
       00 21 M=1,7
       00 TO(17,19,17,19,19,17,19)M
   17 00 3 N=1,33
     3 CB2(M/N)=((TO/T(N))+41.5)
       00 TO 21
   19 00 4 N=1,33
     4 CB2(MAN)=TO/T(N)
    21 CONTINUE
CC
       FACTOR GIVING TEMPERATURE AND PREBBURE DEPENDENCE OF LINE WIOTH IB
       COMPUTED AT EACH ALTITUDE
       00 5 N=1/33
     5 CA(N)=((TO/T(N))++0+5)+(P(N)/PO)
       DOP1(N1,NE) IS A FACTOR NECESBARY TO DETERMINE THE DOPPLER
       BROADENING FOR A GIVEN MOLECULE AT A GIVEN ALTITUDE
       00 372 N1=1,7
00 372 N2=1,33
  372 DOP1(N1,N2)=DOP(N1)+T(N2)+++5
       SUM-0.0
       BAVE-0.0
       V-V1
```

C

```
START OF COMPUTATION OF ATTENUATION AT A FIXED ALTITUDE AND
 C
 C
        FIRST THE INDEX OF THE LINES THAT LIE WITHIN PLUS OR MINUS SOUND
 C
       OF THE FREQUENCY OF INTEREST ARE DETERMINED
    25 DO 33 I-15,11
       IF ( V-BOUND-QNU( I ) )29, 29, 33
    29 15-1
       00 TO 35
    33 CONTINUE
       IS-I1
       00 TO 53
    35 00 39 J-15,11
       IF(V+80UND=QNU(J))37,37,39
    37 I6-J-1
       GO TO 43
   39 CONTINUE
       16-11
   43 00 6 N=1,33
      00 27 Mal, 7
      CAY1 (M) -0.0
   27 SUM1(M)=0.0
      DO 23 I-15,16
      M-MOL(I)
      88-8(I)+C82(M/N)+(EXP(-EOP(I)+C81(N)))+(1.-EXP(-4.86378E-03+GNU(
     11115
      IF IC-O ALL CONSTITUENTS ARE TAKEN INTO ACCOUNT, IF IC-M ONLY
      CONSTITUENT MAIF ICOOM ALL BUT CUNSTITUENT M
IF(IC.GT.O.AND.M.NE.IC.OR.IC.EG.(OM))88-0
      ALPHA1-ALPHA(I)+CA(N)
      MeMOL(I)
     Z-V-QNU(I)
     LPoLP1
     IF THE FREQUENCY AT WHICH THE ATTENUATION IS COMPUTED IS
     HITHIN . 0005 CHOOL OF A LINE THE VOIGT PROFILE AT THE CENTER
     OF THAT LINE IS USED AND THIS FACT IS OUTPUT
     IF (ABB(Z) -LE - - 0005 - ANO - N - EQ - 1 | OUTPUT (108) Z
     IF (ABS(Z) . LE . . DOOS) LP-4
     Z1-V+ONU(I)
     SRANCH TO DIFFERENT CALCULATIONS DEPENDING ON LINE SHAPE
     00 TO(200,201,202,203),LP
     LORENTZ LINE SHAPE
200 SUM1(M)-88-AL(10)1/(Z-+2+ALPHA14-Z)
    00 TO 225
    VAN=VLECK WEISSKOPF LINE SHAPE
201 VVHF=(1/(Z++2+ALPHA1++2))+(1/(Z1++2+ALPHA1++2))
    SUM1 (M)=(88+ALPHA1+(V4+2)/(GNU(1)++2))+VVHF
    00 TO 225
    'KINETIC'(GROSS/ZHEVAKIN-NAUHOV) LINE SHAPE
202 GRa((Z+Z1)+02)+(4++(V++2)+(ALPHA1++2))
    SUM1(M)-SS+ALPHA1+4++(V++2)/GR
    00 TO 225
    NEXT THE COPPLER HIDTH FOR THE GIVEN LINE IS CALCULATED
203 SETA-GNU(I)-00P1(M,N)
```

```
THE NEXT PARAMETER DEPENDS ON THE RATIO OF THE COLLISIONALLY
      BRUADENED HIOTH TO THE DOPPLER WIDTH
C
      Y-ALPHA1/BETA
      DEPENDING ON THE ABUVE PARAMETER EITHER AN ASYMPTOTIC FORMULA
C
      FOR THE VOIGT PROFILE AT THE CENTER OF A RESONANCE LINE IS USED
C
      OR A POLYNOMIAL APPROXIMATION FOR THE PROBABILITY INTEGRAL IS
C
      ADJPTED
      IF (Y+GE+5+190 TO 204
      TY-1-/(1++-3275911+Y)
      TYZOTYOTY
      TY3-TY2+TY
      TY4=TY3+TY
      TYS=TY4+TY
      SUM1(M)=55+1.772454+(.2548296+TY=.2844967+TY2+1.421414+TY3
     2-1.453152+TY4+1+061+05+TY5)/BETA
      GO TO 225
  204 Y2-Y4Y
      YASYETY
      Y4-Y3-Y
      Y5-Y44Y
      76-Y5-Y
       Y7-Y6-Y
       YB-Y7-Y
      YSSYSSY
      SUM1(M)=SS+(1-77-+5/Y3++75/Y5-1-875/Y7+6+5425/Y9)/BETA
  225 CAY1(M)+C4Y1(M)+BUM1(M)
   23 CONTINUE
      CAY=0 0
DO 47 M=1,7
   47 CAY=CAY+CAY1(M)+W(MAN)
      OPJ-CAY+1 . 38240
       IF(N.EQ.1)G0 TO 10
                          IN AT THE VARIOUS LEVELS IS SUMMED
       NEXT THE ATTEN
                         (N=1))+(CPD+BAVE)
       SU-SUM+ . 5+1
                        KIND IVIOPO
   10 DOLYINATVINSUI
      S/ . " JPO
    & C .NUE
      Fig. IZVIOV
       DO 109 N=1,33
  109 UP(NJIV)-SUM-DOWN(NJIV)
       IF( ( V+0 V ) . GT . V2P ) GO TO 53
       IF((V+.5+DV).GE.V2)40 TO 53
       IF( IV . GE . 100 ) GO TO 53
       IV=IV+1
       THE FREQUENCY IS INCREMENTED AND THE CALCULATION PERFORMED AGAIN
       V=V1+(1V=1)+DV
       SUM-0.0
       SAVE-0.0
       60 TO 25
   53 GO TO(215,214,217),LP1
  215 WRITE(111,101) IV, V, V2P, IC
       60 TO 219
                           LORENTZ PROFILE', 3x, 'CONSTITUENT", 15)
  101 FORMAT(15,2F10.4,
  216 WRITE(111,220) IV, V, V2P, IC
```

```
GO TO 219
  220 FORMAT(15,2F10.4,1
                          VAN VLECK-WEISSKOPF PROFILE', 3X, 'CONSTITUENT"
     2', 151
  217 WRITE(111,221) IV, V, V2P, IC
  221 FORMAT(15,2F10.4, ' GROSS PROFILE',3X, 'CONSTITUENT",15)
  112 FORMAT(413,4F8.2,4X,11,13,1(07.2)1,10X,F8.2)
  219 FINAL=V1+99++DV
      DO 107 J=1, IV
C
      THE NEXT STATEMENTS GENERATE AN OUTPUT FILE TO BE USED AS INPUT FOR
      A GRAPHICE ROUTINE CALLED OPLOTID
      WRITE(109,110)10,0,0,0
 110 FORMATIAIS, 'HORIZONTAL AND VERTICAL MULECULAR ATTENUATION'S
      WRITE(109,111)10,0,0,0,0,(MODEL(KK,MOD),KK-1,7),FNU(J),BOUNG
 111 FORMAT(413,644,42, 'FREQ=',F8.3,' CM*+=1',' BOUNO=',F7.3,' CM++=1'
     GO TO(210,211,212), LP1
 210 WRITE(109,124)10,0,0,0,10
     00 TO 218
 124 FORMAT(413, 'O-DOWN(DB) U-UP(DB) H-HOR(OB/KM) LORENTZ', 2X, ' CON
    28TITUENT- ', IS)
 211 HRITE(109,214)10,0,0,0,1C
 214 FORMAT(413, '0-00WN(DE:
                             U-UP(08) H-HOR(08/KM) VAN VLECK-WEIBSKOP
    2F',3X,'CON=',IS)
     GO TO 218
 212 WRITE(109,213)10,0,0,0,1C
 213 FORMAT(413, '0-DOWN(DE) U-UP(OB) H-HOR(OB/KM) GROSS',2X,' CONST
    ZITUENT-1, IS)
 218 WRITE(109,112)2,0,1,1,.7,70.,.2,.2,1,3,.1
     WRITE(109,180)2,90,1,1,1.,1000.,.2,.2,1,8,.1
 15C FORMAT(413,2F8.0,2F8.2,4X,[1,13,'(G8.3)',10X,F8.2)
     WRITE(109,113)4,1,-1,0,-1,0,0
 113 FORMAT(713)
     WRITE(109,114)3,0,1,+30,0
 114 FORMATIBIS)
     WRITE(109,115)(H(NN),NN=2,31)
 115 FORMAT(10F8.0)
 116 FORMATIZISI
     WRITE(109,151)3,90,1,+30,0,1,1,1-,1000+
     WRITE(109,122) . 00WN(NN,J),NN=2,31)
122 FORMAT(10(08.3))
     WRITE(109,114)5,+2,68,0
     WRITE(109,151)3,90,1,+30,0,1,1,1.,1.,1000.
     WRITE(109,122)(UP(NN,J),NN=2,31)
    WRITE(109,114)5,+2,85,0
    WRITE(109,154)2,0,1,1,.7,70.,3,3,1,1,.1
154 FORMAT(413,4F8.2,4X,11,13,1(11,-X,11 11)1,5X,F8.2)
    WRITE(109,113)4,-2,0,0,0,0,0
    WRITE(109,152)2,90,1,1, •1,100 •, •2, •2,1,7, •1
152 FORMAT(413,2F8.2,2F8.2,4X,11,13,'(4X,G7.2)',7X,F8.2)
    WRITE(109,113)4,0,-2,0,0,0,0
    WRITE(109,151)3,90,1,+30,0,1,1,+1,100+
151 FORMAT (713,2F8+2)
    WRITE(109,123)(HOR(NN,J),NN=2,31)
123 FORMAT(10(GB.3))
```

```
WRITE(109,114)5,+2,72,0
    WRITE(109, 153)12, 2, 2, 0, 0, 938, 485
153 FORMAT (513,2F8.0, 1
                            DE PER KMI)
    WRITE(109,117)12,0,2,1,0,200,15
117 FORMAT(BI3, 218, 'VERTICAL HEIGHT(KM)')
    HRITE(109,118)12,2,2,+1,0, 5,665
118 FORMAT(BI3, 218, 'ATTENUATION OB')
    WRITE(109,114)1
    THE NEXT STATEMENTS GENERATE A TABULAR OUTPUT
    WRITE(111)104)FNU(J)
106 FORMAT ( 'FREQUENCY-'>F10.3)
    WRITE(111,104)
104 FORMATIZE! HEIGHT
                            HOR
                                        DOWN
                                                             . 11
107 WRITE(111,108)(H(NN),HOR(NN,J),OUNN(NN,J),UP(NN,J),NN=1,33)
105 FORMAT(2(F10.3,3E12.5))
    IF((V++8+0V)-0E-V2)90 TO 75
    IF((V+DV) . GT . V2P1GO TO 67
    IF(V.GE.FINAL)GO TO 63
    90 TO 75
63 VIOFINAL+OV
    15-1
   IV-1
   V-V1
    00 TO 25
   NEXT THE DATA FROM THE DATA FILE WILL BE REORGANIZED AND THE FILE
   WILL BE READ AGAIN
67 IV-1
   V1-V+DV
   VBOT-V1-BOUND
   DO 69 IN-1,11
   IF (ONU(IN) . GT . VBOTIGO TO 71
69 CONTINUE
   IN-I1
71 IJ=IN
   L-1
00 73 I-IJ, I1
   ONU(L)-GNU(I)
   B(L)-B(I)
   ALPHA(L)-ALPHA(I)
   EOP(L)-EOP(I)
   MOL(L)=MOL(I)
73 L-L+1
   ILL
   ILL-L
   00 TO 1
75 CALL EXIT
   END
```

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file and atmospheric model can be selected from among several. Comparison is made with other calculations and with experiment	A computer programment on the attenuation by arradiation space is calculation.	cossery and identify by block numberion cossery and identify by block numbering (SLAM) is described for microwave are the horizontal attainus levels down thated for fixed free	eribed which calculates and submillimeter wave cenuation, the vertical to the ground and out equency. The line pro-

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